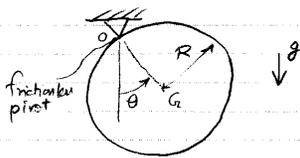


Solution by Basant Sharma

April 12 '02.

Q 7.134

Thin hoop of radius R and mass M hung from a point O on its edge.



a) FBD of hoop

AMB_O: $\dot{H}_O = Mv_O$

$\dot{H}_O = \int r \times R dm$
hoop, origin O

$= \int r \times (-r\dot{\theta}\hat{e}_1 + r\dot{\theta}\hat{e}_2) dm$

$= \int r\hat{e}_1 \times (-r\dot{\theta}\hat{e}_1 + r\dot{\theta}\hat{e}_2) dm$

$= \int r^2 \dot{\theta} \hat{k} dm$

$= \dot{\theta} \int (r^2) dm \hat{k} = \dot{\theta} \int (R^2 + y^2) dm \hat{k}$

$= \dot{\theta} (\int R^2 dm + 2 \int y \cdot R dm + \int y^2 dm) \hat{k}$

$= \dot{\theta} (MR^2 + \int y^2 dm) \hat{k}$

$= \dot{\theta} (MR^2 + MR^2) \hat{k} = 2MR^2 \dot{\theta} \hat{k}$

$Mv_O = -MgR \sin \theta \hat{k}$

So by AMB: $2MR^2 \dot{\theta} = -MgR \sin \theta$ (1)

Assume θ is small for oscillation - in-plane considered, so $\sin \theta \approx \theta$

(1) $\Rightarrow \ddot{\theta} + \frac{g}{2R} \theta = 0$ (2)

Compare (2) with simple harmonic oscillator, so

Time period $= \frac{2\pi}{\sqrt{g/2R}} = 2\pi \sqrt{\frac{2R}{g}}$ (T1)

b) FBD of hoop

AMB_O: $\dot{H}_O = Mv_O$

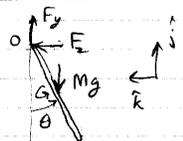
$\dot{H}_O = I_{xx/O} \dot{\theta} \hat{k}$

with $I_{xx/O} = \frac{1}{2} I_{zz/G} + MR^2$

$= \frac{3}{2} MR^2$

(by Parallel axis and Perpendicular axis theorem)

$Mv_O = -MgR \sin \theta \hat{k}$



AMB: $\hat{k} \Rightarrow \frac{3}{2} MR^2 \ddot{\theta} = -MgR \sin \theta$ (3)

Assume θ small, so $\sin \theta \approx \theta$

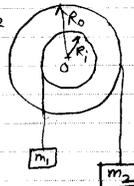
(3) $\Rightarrow \frac{\ddot{\theta} + \frac{2g}{3R} \theta = 0$ (4)

So Time period $= \frac{2\pi}{\sqrt{2g/3R}} = 2\pi \sqrt{\frac{3R}{2g}}$ (T2)

Comparing T1 and T2 we can see that the period of oscillation is less in the case of in and out of plane swinging (second case) as against inplane swinging (first case)

Q 7.141

$R_i = 0.2m, R_o = 0.4m, I_o = 2.7kgm^2$
 $m_1 = 40kg, m_2 = 100kg$



a) FBD of pulley

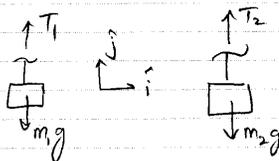
AMB_O:

$\dot{H}_O = Mv_O$

So $\{I_O \dot{\alpha} \hat{k} = (T_1 R_i - T_2 R_o) \hat{k}\}$

$\{ \hat{k} : I_O \alpha = T_1 R_i - T_2 R_o$ (1)

FBD of masses m1 and m2



LMB: $m_1 a_1 = (T_1 - m_1 g) \hat{j}, m_2 a_2 = (T_2 - m_2 g) \hat{j}$

By kinematics: $a_1 = a_A = +\alpha \hat{k} \times R_i (\hat{i}) = -R_i \alpha \hat{j}$
 $a_2 = a_B = \alpha \hat{k} \times (R_o \hat{i}) = R_o \alpha \hat{j}$

So $\begin{cases} m_1 R_i \alpha \hat{j} = (T_1 - m_1 g) \hat{j} \\ m_2 R_o \alpha \hat{j} = (T_2 - m_2 g) \hat{j} \end{cases}$

$\{ \hat{j} : \Rightarrow \begin{cases} T_1 = m_1 (g - R_i \alpha) \\ T_2 = m_2 (g + R_o \alpha) \end{cases}$ (2)

(1) and (2) give

$\alpha = \frac{(m_1 R_i - m_2 R_o) g}{I_O + (m_1 R_i^2 + m_2 R_o^2)}$

Using data

$\alpha \approx -15.45 \text{ rad/s}^2$ (3)

b) by (2), (3) and data

$T_1 \approx 515.6 \text{ N}$

$T_2 \approx 362 \text{ N}$

Q 7.143

Given $R_A = 400 \text{ mm}$
 $R_B = 200 \text{ mm}$

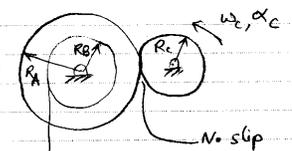
Combined $I_O = 0.5 \text{ kgm}^2$
of A, B

$R_C = 300 \text{ mm}$

$m = 5 \text{ kg}$

$\omega = 60 \text{ rpm} = 2\pi \text{ rad/s}$

$\alpha = 12 \text{ rpm/s} = \frac{2\pi}{5} \text{ rad/s}^2$



acceleration of mass m $a = ?$

By kinematics,

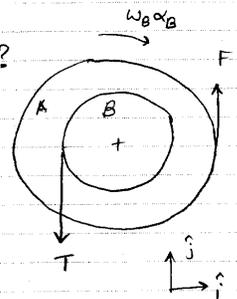
$a = \alpha_B \hat{k} \times (-R_B \hat{i}) = -R_B \alpha_B \hat{j}$

and $R_C \omega_C = R_A \omega_B$
 $R_C \alpha_C = R_A \alpha_B$

So $a = -R_B \left(\frac{R_C}{R_A} \right) \alpha_C \hat{j}$

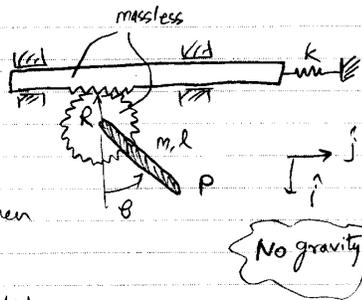
Using data $a = -\frac{3}{20} \times \frac{2\pi}{5} \hat{j} \text{ m/s}^2$

$a \approx -0.188 \text{ m/s}^2$



Q 7.149

(rack and gear)
Spring relaxed when $\theta = 0$.
at $t=0$, $\theta = \theta_0$.
acceleration of P (when $\theta = 0$) = ?



No gravity

FBD of gear with stick:

AMB: $\dot{H}_O = \dot{M}_O$

$\dot{H}_O = I_{zz/O} \ddot{\theta} \hat{k}$

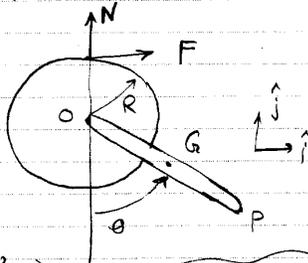
$(I_{zz/O} = I_{zz/G} + m(\frac{l}{2})^2$

$= \frac{ml^2}{12} + \frac{ml^2}{4} = \frac{ml^2}{3}$

Using parallel axis theorem

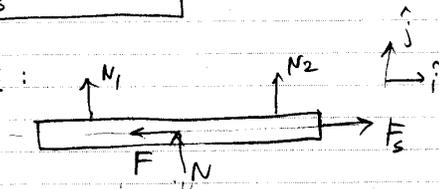
$\dot{M}_O = -FR \hat{k}$

(AMB) $\cdot \hat{k}$: $\frac{ml^2}{3} \ddot{\theta} = -FR$ (1)



Since gear is massless we need only $I_{zz/O}$ of rod.

FBD of rack:



(LMB) $\cdot \hat{i}$: $F_s - F = m a_x$
(\because rack is massless)

$\therefore F = F_s$ (2)

By kinematics the stretch in spring unstretched

$\Delta x = R\theta$

So $F_s = k\Delta x = kR\theta$

\therefore (2) $\Rightarrow F = kR\theta$



By (1) $\frac{ml^2}{3} \ddot{\theta} = -kR\theta$ (1')

Since $\theta(0) = \theta_0$, $\dot{\theta}(0) = 0$ (rests at $t=0$)

$\theta(t) = \theta_0 \cos(\sqrt{\frac{3kR}{ml^2}} t)$

So the slide first crosses $\theta=0$ at $t = \frac{\pi/2}{\sqrt{3kR/ml^2}}$

In general, $\theta=0$ when $t = \frac{(2n+1)\pi/2}{\sqrt{3kR/ml^2}}$, n any integer.

Now $\dot{\theta}(t) = -\theta_0 \sqrt{\frac{3kR}{ml^2}} \sin(\sqrt{\frac{3kR}{ml^2}} t)$

So when $\theta=0$, $\dot{\theta}^2 = \theta_0^2 \frac{3kR}{ml^2}$ (3)

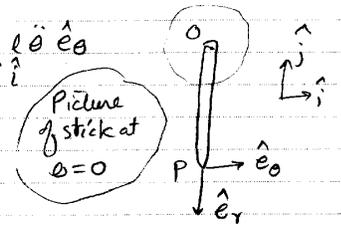
Clearly by (1'), when $\theta=0$, $\ddot{\theta} = 0$ (4)

By rigid body kinematics, when $\theta=0$

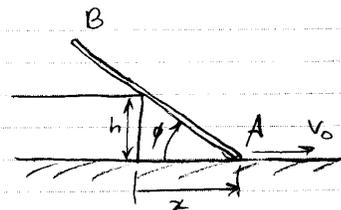
$a_P = -l\dot{\theta}^2 \hat{e}_r + l\ddot{\theta} \hat{e}_\theta$
 $= -l\dot{\theta}^2 (-\hat{j}) + l\ddot{\theta} \hat{i}$

by (3), (4)

$a_P = \frac{3kR}{ml} \theta_0^2 \hat{j}$



Q 8.1



Clearly only two quantities change with time here x, ϕ . ie. $x = x(t)$
 $\phi = \phi(t)$.

Since $h = x \tan \phi$ is constant

$x(t) = h \cot \phi(t)$

$\therefore \frac{dx(t)}{dt} = h \frac{d \cot \phi(t)}{dt}$ (use chain rule)
 $= h \frac{d \cot \phi}{d\phi} \bigg|_{\phi=\phi(t)} \cdot \frac{d\phi(t)}{dt}$

$\therefore \dot{x}(t) = -h \operatorname{cosec}^2 \phi(t) \dot{\phi}(t)$ (1)

Given $\dot{x}(t) = v_0 = \text{constant}$

So $\dot{\phi}(t) = \frac{-v_0}{h \operatorname{cosec}^2 \phi(t)} = \frac{-v_0}{h(1 + \cot^2 \phi(t))}$

$\therefore \dot{\phi}(t) = \frac{-v_0}{h(1 + (x/h)^2)} < 0$ (2)

Differentiating (2) w.r.t t , $\ddot{\phi} = \frac{-(v_0)}{h(1 + (x/h)^2)^2} \cdot \frac{2x}{h^2} \dot{x}$

Using $\dot{x} = v_0$, $\ddot{\phi} = \frac{2v_0^2 x}{h^3(1 + (x/h)^2)^2} > 0$