

# 1 Write three matlab functions that solve the general spring-mass IVP

We will consider the generalized linear system without damping which has an invertible mass matrix:

$$M\ddot{\vec{x}} + K\vec{x} = 0 \quad (1)$$

**a** `[tarray xarray] = SpringmassNUM(tspan,x0,v0,K,M)`

This can use ODE45 or your own ODE integrator, your choice. It should work with arbitrary positive definite symmetric  $M$  and  $K$  matrices of any size.

Equation 1 can be rearranged to form Equation 2, which can be numerically integrated. To do this, the equation is first converted into two first order equations, as seen below.

$$\ddot{\vec{x}} = -M^{-1}K\vec{x} \quad (2)$$

$$\vec{z} = \dot{\vec{x}} \quad (3)$$

$$\dot{\vec{z}} = \ddot{\vec{x}} = -M^{-1}K\vec{x} \quad (4)$$

It is worth noting that this is a linear system, and as such can be simulated in Matlab using `lsim()` both faster and more accurately than using any numerical integration method. However, the code below uses `ode45()`.

```
1 function [tarray xarray] = SpringmassNUM(tspan,x0,v0,K,M)
2 % Numerically solves for the motion of the system defined by:
3 %     M(xddot) + K x = 0
4 %
5 % Inputs:
6 %     M,K - Matrices as defined in the equation above
7 %     x0 - vector of initial positions
8 %     v0 - vector of initial velocities
9 %     tspan - times at which to output the state of the system. tspan must be
10 %         a vector of length ≥ 2. The simulation will begin at time in the
11 %         first element of tspan and end at the time in the last element.
12 % Outputs:
13 %     tarray - array of times corresponding to xarray
14 %     xarray - array of system states. The i'th row corresponds to the state
15 %         of the system at the i'th element in tspan
16
17 % Make IC vectors column
18 x0 = x0(:);
19 v0 = v0(:);
20 z0 = [x0; v0];
21
22 n = length(x0);
```

```

23 % Define rhs function - returns the derivative of the state
24 % Because anonymous functions
25 zdot = @(t,z) [z(n+1:end); -M^-1*K*z(1:n)];
26
27 % Use ode45 to integrate
28 [tarray,xarray] = ode45(zdot,tspan,z0);
29 xarray = xarray(:,1:n); % only keep positions
30 end

```

## b [tarray xarray] = SpringmassMinv(tspan, x0,v0,K,M)

This should use a superposition of normal mode solutions based in either (your choice)  $\text{eig}(K,M)$  or  $\text{eig}(M^{-1}K)$ .

First, we rearrange Equation 1 slightly, forming Equation 5.

$$\ddot{\vec{x}} + M^{-1}K\vec{x} = 0 \quad (5)$$

This is the form of the harmonic oscillator equation. Thus, we expect to see oscillatory solutions composed of sines and cosines. Our assumed solution will be written:

$$\vec{x}(t) = x(\omega t)\vec{v} = (A\cos(\omega t) + B\sin(\omega t))\vec{v} \quad (6)$$

Substituting in:

$$(-\omega^2 I + M^{-1}K)x(\omega t)\vec{v} = 0 \quad (7)$$

Since  $x(\omega t)$  is just a scalar, it can be divided out. The result is exactly the eigenvalue problem for the matrix  $M^{-1}K$ , producing  $n$  eigenpairs ( $\lambda_i = \omega_i^2, \vec{v}_i$ ). Each of the  $n$  pairs represents a valid form for our assumed solution in Equation 6. Since the sum of solutions to a homogeneous differential equation is also a solution to that differential equation, we can write the general form of the solution to Equation 5 as:

$$\vec{x}(t) = \sum_{i=1}^n \vec{v}_i (A_i \cos(\omega_i t) + B_i \sin(\omega_i t)) \quad (8)$$

To find the constants  $A_i$  and  $B_i$ , we will make use of the initial conditions:  $\vec{x}(0) = \vec{x}_0$  and  $\vec{v}(0) = \vec{v}_0$ . Applying these conditions, we get the equations:

$$\vec{x}_0 = \sum_{i=1}^n \vec{v}_i A_i = V\vec{A} \quad (9)$$

$$\vec{v}_0 = \sum_{i=1}^n \vec{v}_i \omega_i B_i = V\Lambda^{1/2}\vec{B} \quad (10)$$

where  $V = [\vec{v}_1|\vec{v}_2|\dots|\vec{v}_n]$  and  $\Lambda$ , having the eigenvalues  $\lambda_i$  on its diagonal, are the matrices output by the  $\text{eig}()$  function and we have simply defined vectors  $\vec{A}$  and  $\vec{B}$  to contain the

coefficients  $A_i$  and  $B_i$ , respectively. Noting the fact that  $V^{-1} = V^T$  and solving for these coefficients, we obtain:

$$\vec{A} = V^T \vec{x}_0 \quad (11)$$

$$\vec{B} = \Lambda^{-1/2} V^T \vec{v}_0 \quad (12)$$

Using these results with Equation 8, we have the analytical solution to Equation 1.

```

1 function [tarray xarray] = SpringmassMinv(tspan,x0,v0,K,M)
2 % Solves for the motion of the system defined by:
3 %     M(xddot) + K x = 0
4 % using eigenvectors of M^-1*K
5 %
6 % Inputs:
7 %   M,K - Matrices as defined in the equation above
8 %   x0 - vector of initial positions
9 %   v0 - vector of initial velocities
10 %   tspan - times at which to output the state of the system. tspan must be
11 %           a vector of length >= 2. The simulation will begin at time in the
12 %           first element of tspan and end at the time in the last element.
13 % Outputs:
14 %   tarray - array of times corresponding to xarray
15 %   xarray - array of system states. The i'th row corresponds to the state
16 %           of the system at the i'th element in tspan
17
18 % Make IC vectors column
19 x0 = x0(:);
20 v0 = v0(:);
21
22 % Form timespan
23 if length(tspan) == 2
24     tarray = linspace(tspan(1),tspan(2));
25 else
26     tarray = tspan(:)';
27 end
28
29 [V,w2] = eig(M^-1*K);
30 w = sqrt(diag(w2));
31
32 % Solve for coefficients
33 A = V'*x0;
34 B = w2^(-1/2)*V'*v0;
35
36 % Vectorized linear combination of normal modes
37 cospart = repmat(A,1,length(tarray)).*cos(w*tarray);
38 sinpart = repmat(B,1,length(tarray)).*sin(w*tarray);
39 x = V*(cospart + sinpart);
40 xarray = x';
41 end

```

**c** `[tarray xarray] = SpringmassSqrtM(tspan, x0,v0,K,M)`

This should use a superposition of normal mode solutions based on the methods of lecture on 10/18 (using two changes of coordinates)

We can select a set of coordinates  $\vec{q} = M^{1/2}\vec{x}$  and multiply Equation 1 by  $M^{-1/2}$  to obtain:

$$\ddot{\vec{q}} + M^{-1/2}KM^{-1/2}\vec{q} = \ddot{\vec{q}} + \tilde{K}\vec{q} = 0 \quad (13)$$

$\tilde{K}$  has the convenient property that it has orthogonal eigenvectors. As such,  $P^T\tilde{K}P = \Lambda$ , where  $P$  has the eigenvectors of  $\tilde{K}$  as its columns (in the same way  $V$  was defined with respect to  $M^{-1}K$  in Section b) and  $\Lambda$  has the eigenvalues of  $\tilde{K}$  on its diagonal (the are the same as the eigenvalues of  $M^{-1}K$ ). We will exploit this fact by defining a new set of coordinates,  $\vec{r} = P^T\vec{q}$ . These are called “modal coordinates”. We substitute this into Equation 13 and multiply by  $P^T$  to obtain:

$$\ddot{\vec{r}} + P^T\tilde{K}P\vec{r} = \ddot{\vec{r}} + \Lambda\vec{r} = 0 \quad (14)$$

Here we could proceed with the same analysis as in Section b to arrive at solutions for  $\vec{r}(t)$ , but instead, we will recognize that, due to the diagonal nature of  $\Lambda$ , Equation 14 represents a system of  $n$  decoupled differential equations with only a single degree of freedom. Each of these equations can be written as in Equation 15.

$$\ddot{r}_i + \lambda_i r_i = 0 \quad (15)$$

We can now solve each of these  $n$  equations using familiar techniques for 1-DOF oscillators. We can guess the form of the solutions:

$$r_i(t) = C_i \cos(\sqrt{\lambda_i}t) + D_i \sin(\sqrt{\lambda_i}t) \quad (16)$$

In order to apply the initial conditions for our equations, we must convert them to modal coordinates. By the definitions of  $\vec{r}$  and  $\vec{q}$ , we have the transformations between coordinates:

$$\vec{r} = P^T M^{1/2} \vec{x} \quad (17)$$

$$\vec{x} = M^{-1/2} P \vec{r} \quad (18)$$

As such, we can transform the initial conditions with Equation 17 to obtain  $\vec{r}_0 = P^T M^{-1/2} \vec{x}_0$  and  $\dot{\vec{r}}_0 = P^T M^{-1/2} \dot{\vec{x}}_0$ . We apply these initial conditions to Equation 15 to obtain the coefficients as

$$C_i = r_{0,i} \quad (19)$$

$$D_i = \frac{\dot{r}_{0,i}}{\sqrt{\lambda_i}} \quad (20)$$

We have solved for  $\vec{r}(t)$  by finding its individual components. To obtain the solution  $\vec{x}(t)$ , we simply apply the transformation in Equation 18.

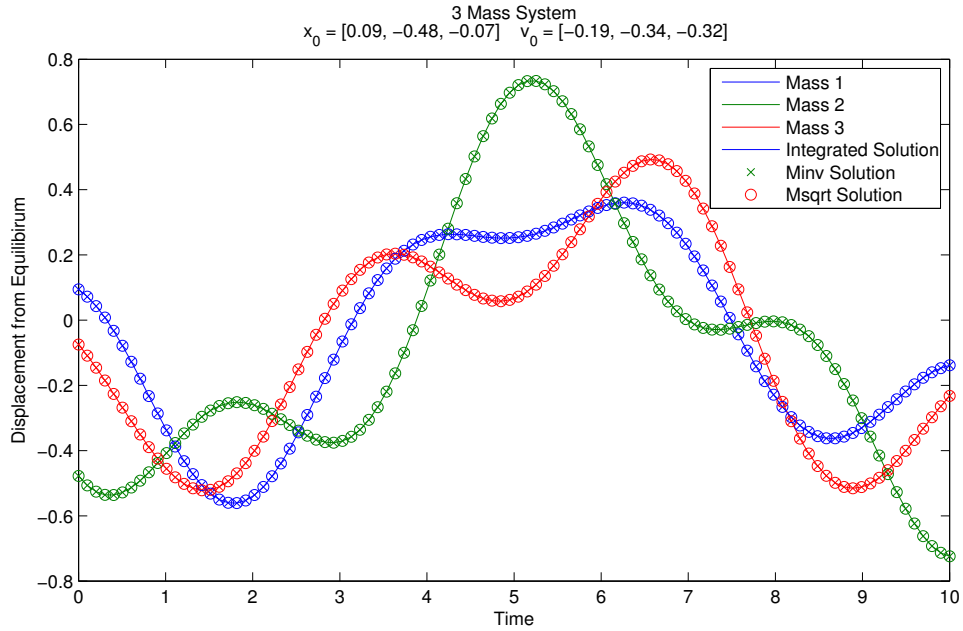
```

1 function [tarray xarray] = SpringmassSqrtM(tspan,x0,v0,K,M)
2 % Solves for the motion of the system defined by:
3 %     M(xddot) + K x = 0
4 % using modal coordinates
5 %
6 % Inputs:
7 %     M,K – Matrices as defined in the equation above
8 %     x0 – vector of initial positions
9 %     v0 – vector of initial velocities
10 %     tspan – times at which to output the state of the system. tspan must be
11 %         a vector of length  $\geq 2$ . The simulation will begin at time in the
12 %         first element of tspan and end at the time in the last element.
13 % Outputs:
14 %     tarray – array of times corresponding to xarray
15 %     xarray – array of system states. The i'th row corresponds to the state
16 %         of the system at the i'th element in tspan
17
18 % Make IC vectors column
19 x0 = x0(:);
20 v0 = v0(:);
21
22 % For time span
23 if length(tspan) == 2
24     tarray = linspace(tspan(1),tspan(2));
25 else
26     tarray = tspan(:)';
27 end
28
29 Msqrt = M^(-1/2);
30 Ktwid = Msqrt*K*Msqrt;
31 [P,w2] = eig(Ktwid);
32 w = sqrt(diag(w2));
33
34 % Transform ICs
35 r0 = P'*Msqrt^-1*x0;
36 rd0 = P'*Msqrt^-1*v0;
37
38 % Solve for coefficients
39 C = r0;
40 D = rd0./w;
41
42 % Solution for each 1DOF oscillator
43 r = repmat(C,1,length(tarray)).*cos(w*tarray) +...
44     repmat(D,1,length(tarray)).*sin(w*tarray);
45
46 % Transform back to x-coordinates
47 x = M*P*r;
48 xarray = x';
49 end

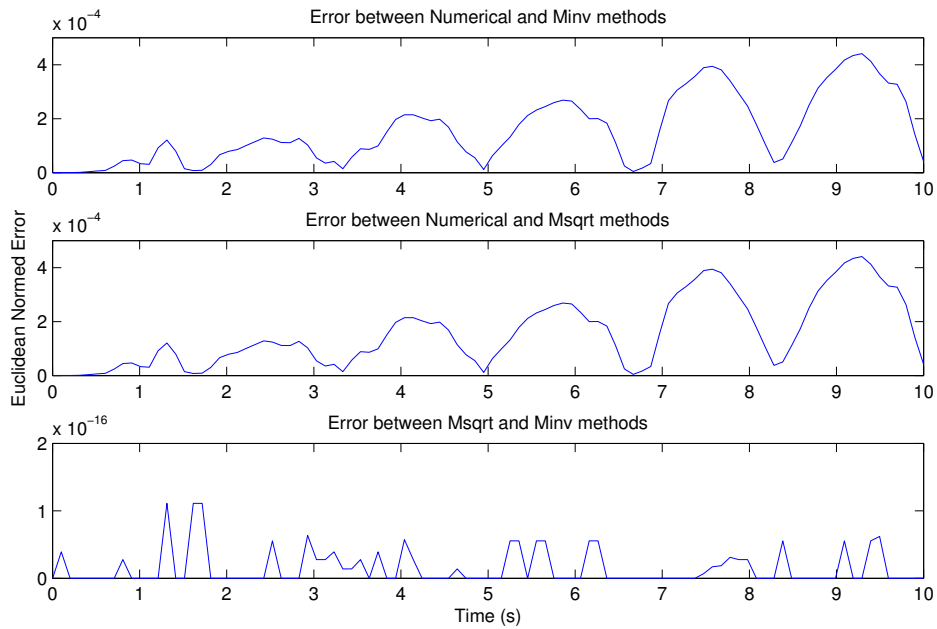
```

**d** For some fairly complex problem show that your three methods agree as well as they should.

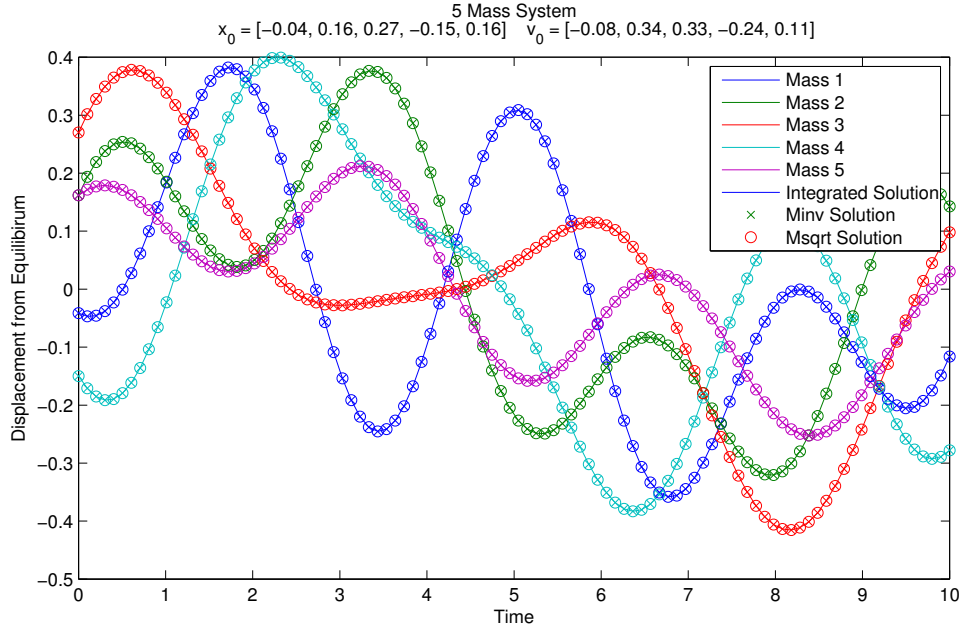
This comparison includes the functions described below in Section 2.



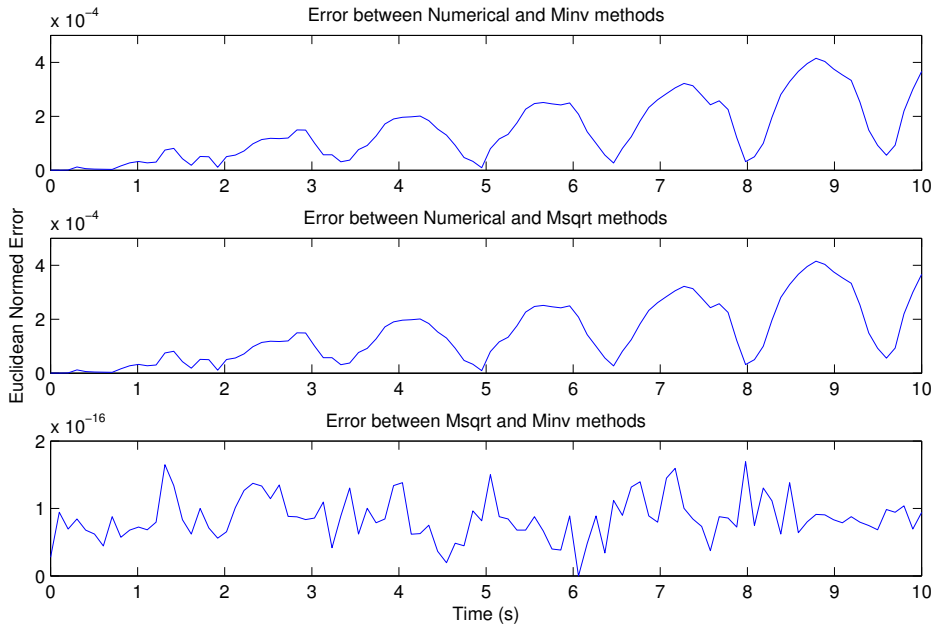
**Figure 1:** Solutions for a three mass system with a nonsingular K matrix using the methods described above that do not handle singular matrices.



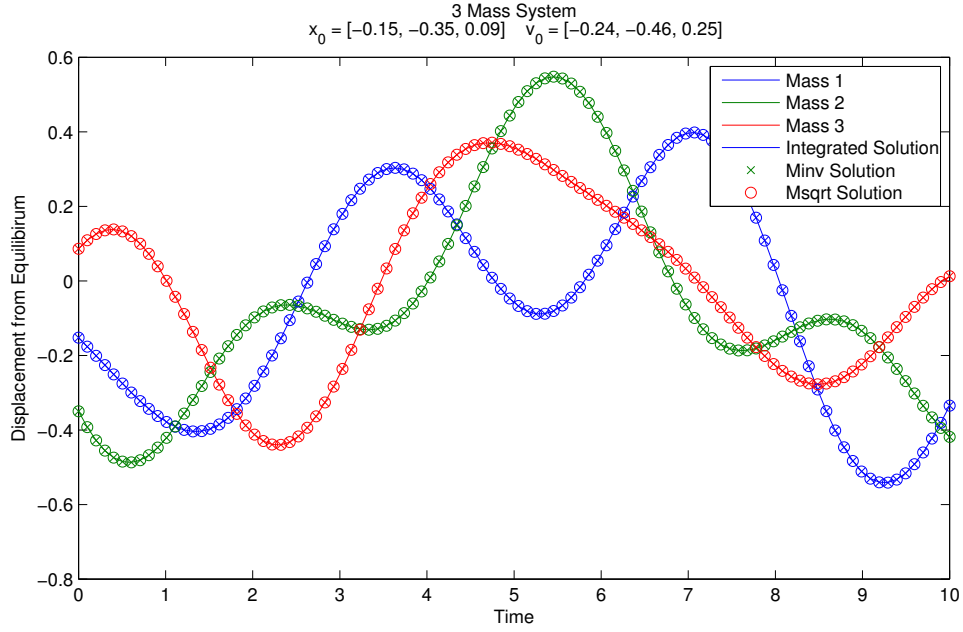
**Figure 2:** Associated error for the system in Figure 1



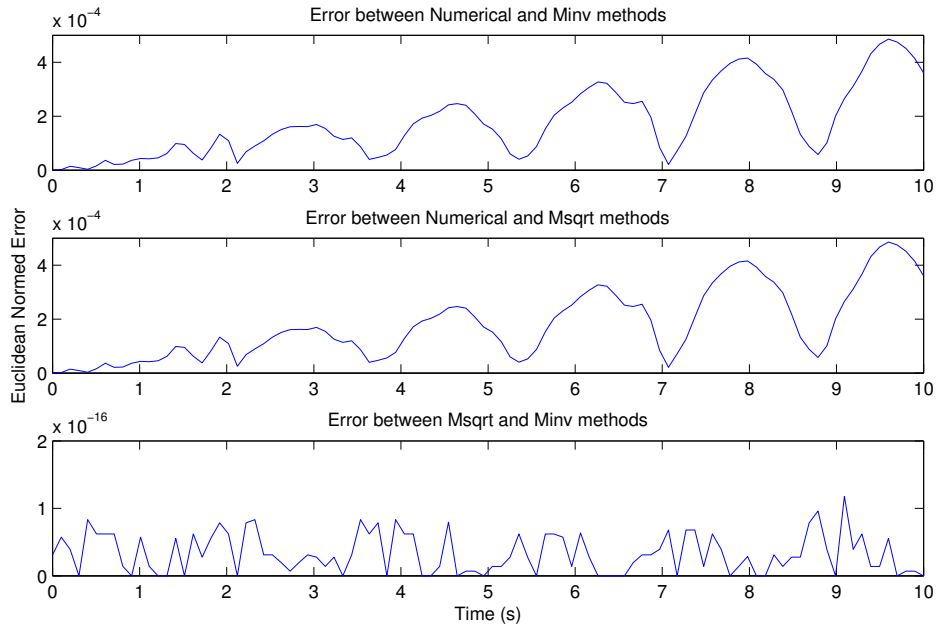
**Figure 3:** Solutions for a five mass system with a nonsingular K matrix using the methods described above that do not handle singular matrices. Note that this system is not simply five masses connected with springs in series, but instead has some springs that connect non-adjacent masses.



**Figure 4:** Associated error for the system in Figure 3

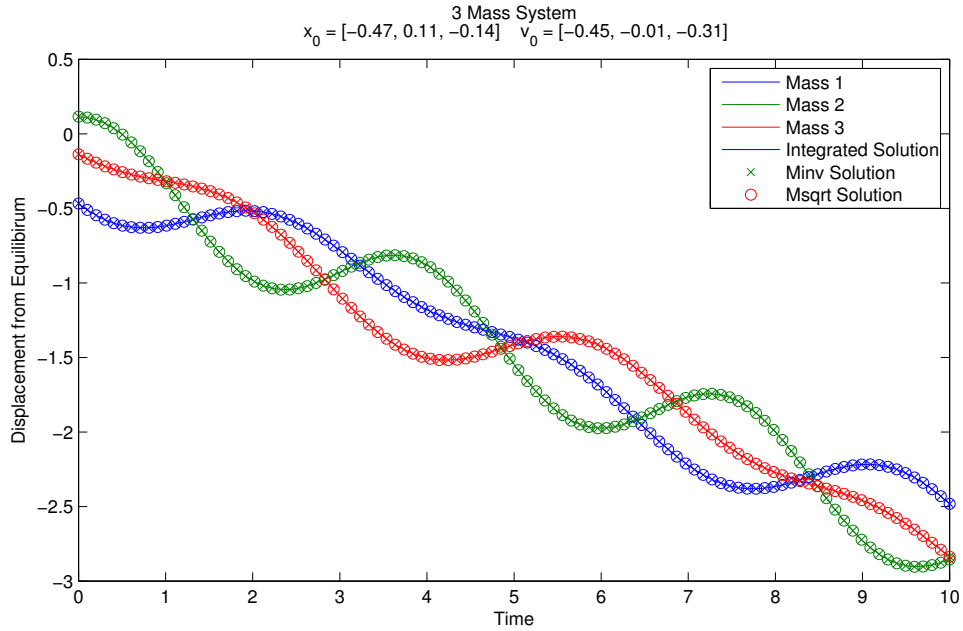


**Figure 5:** Solutions for a three mass system with a nonsingular  $K$  matrix using the methods described below that employ sine and cosine functions to find the motion when  $K$  may be singular.

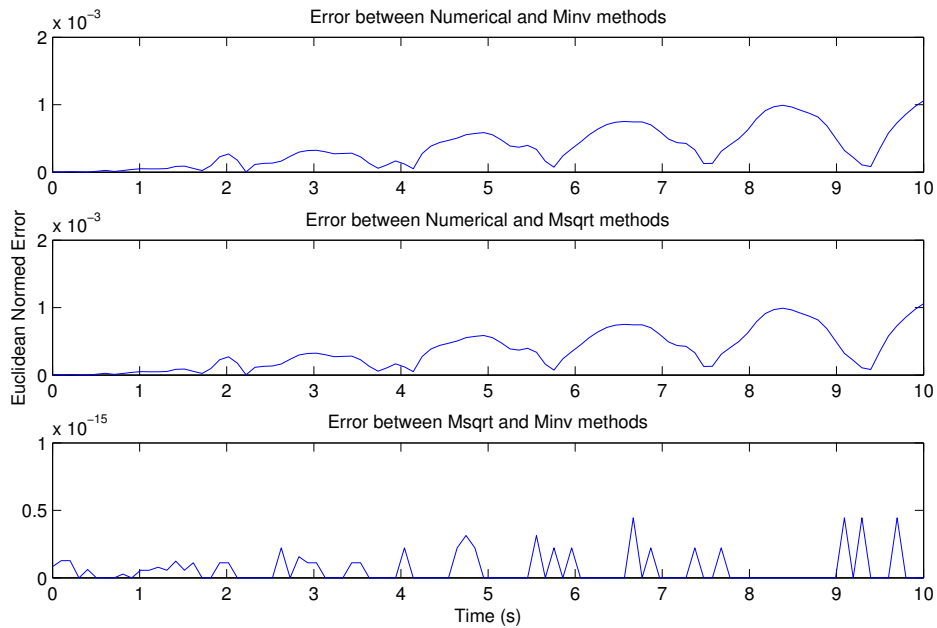


**Figure 6:** Associated error for the system in Figure 5

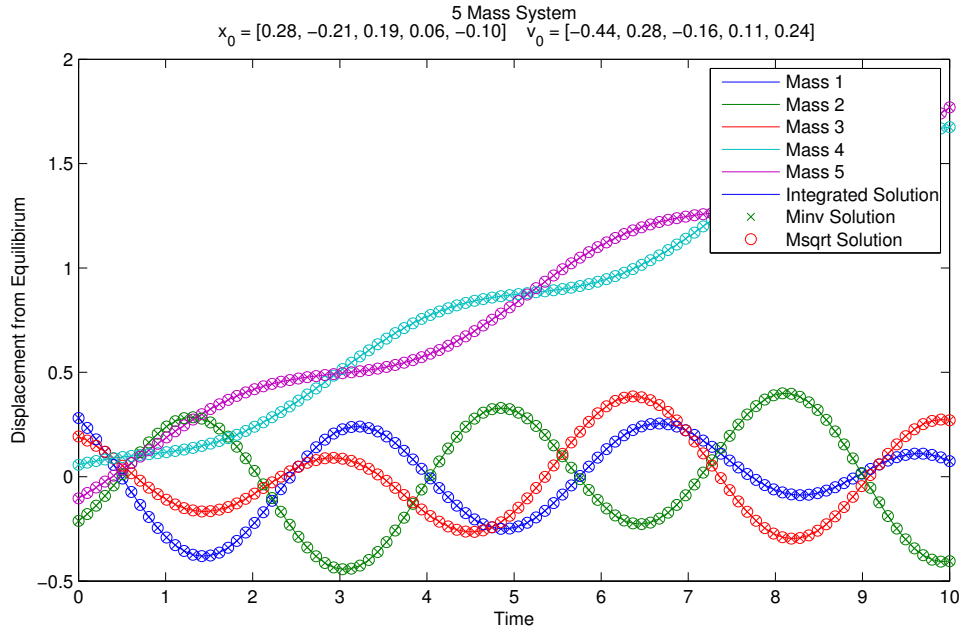




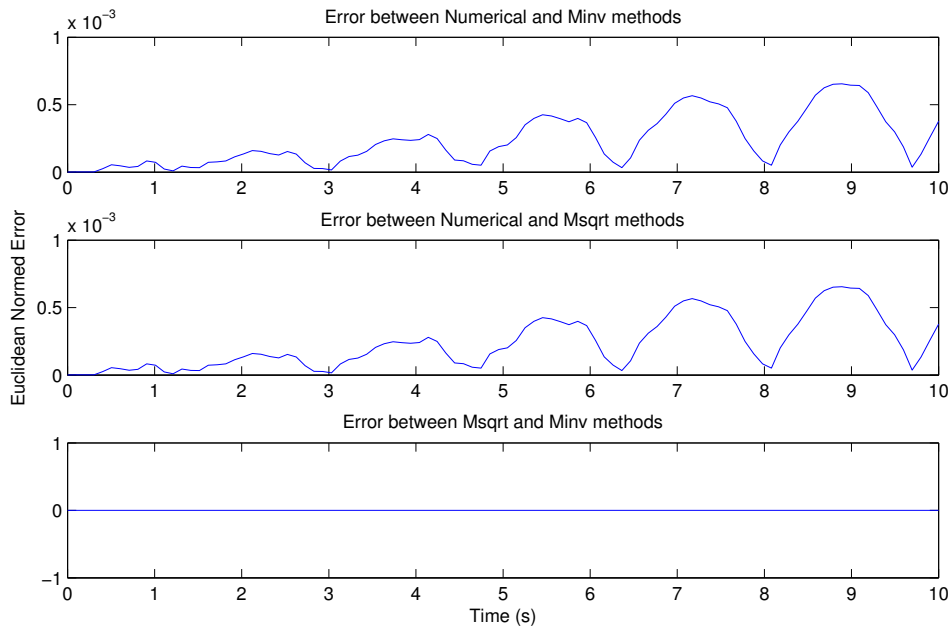
**Figure 7:** Solutions for a three mass system with a singular  $K$  matrix using the methods described below that employ sine and cosine functions to find the motion when  $K$  may be singular.



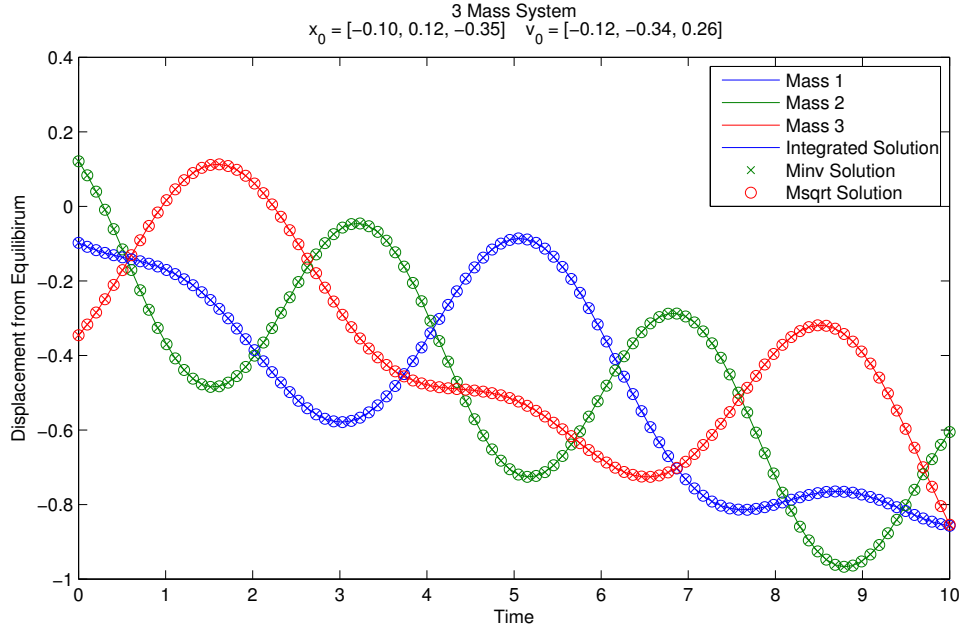
**Figure 8:** Associated error for the system in Figure 7



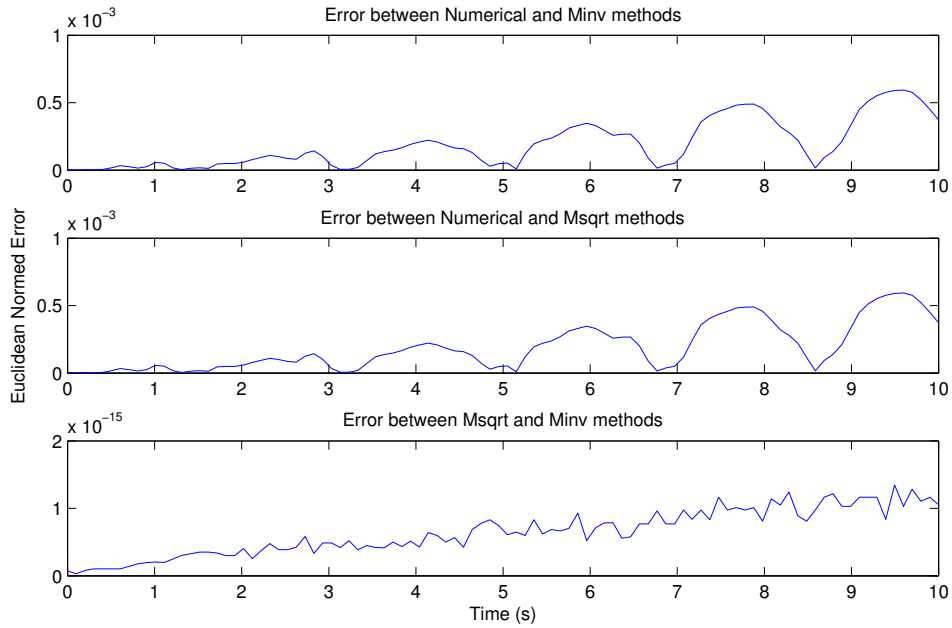
**Figure 9:** Solutions for a five mass system with a singular K matrix using the methods described below that employ sine and cosine functions to find the motion when K may be singular.



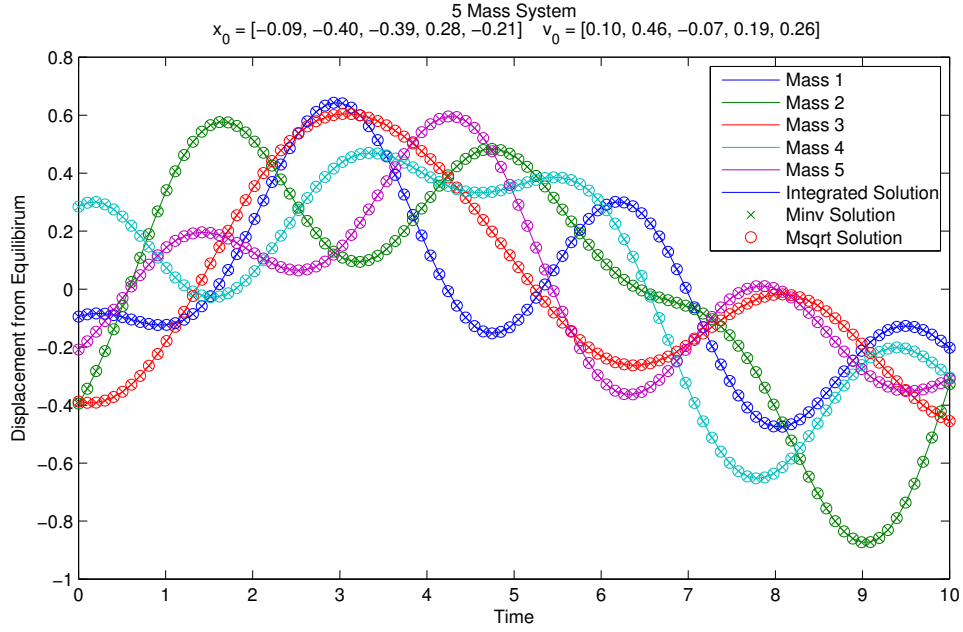
**Figure 10:** Associated error for the system in Figure 9



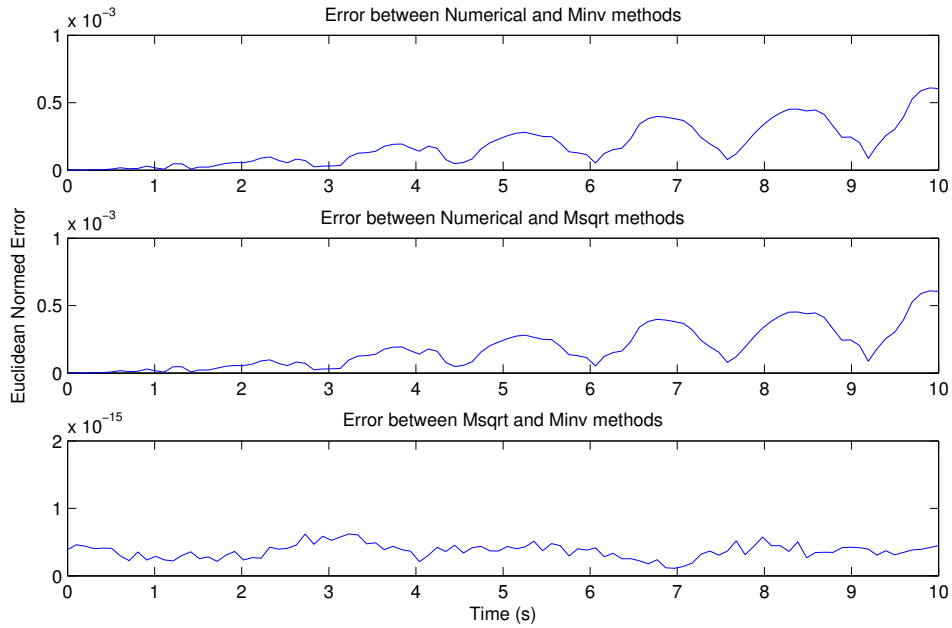
**Figure 11:** Solutions for a three mass system with a singular  $K$  matrix using the methods described below that employ exponential functions to find the motion when  $K$  may be singular.



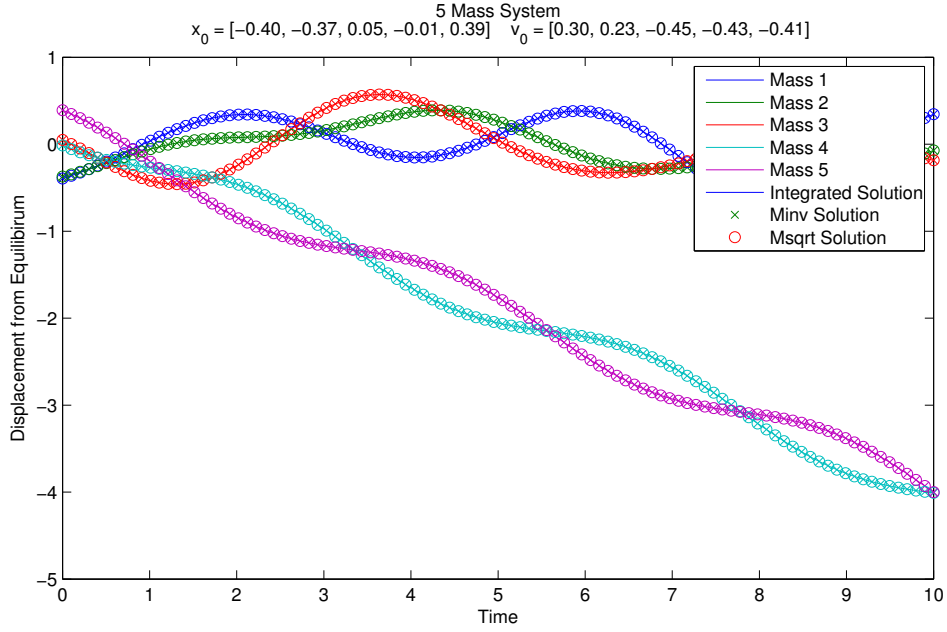
**Figure 12:** Associated error for the system in Figure 11



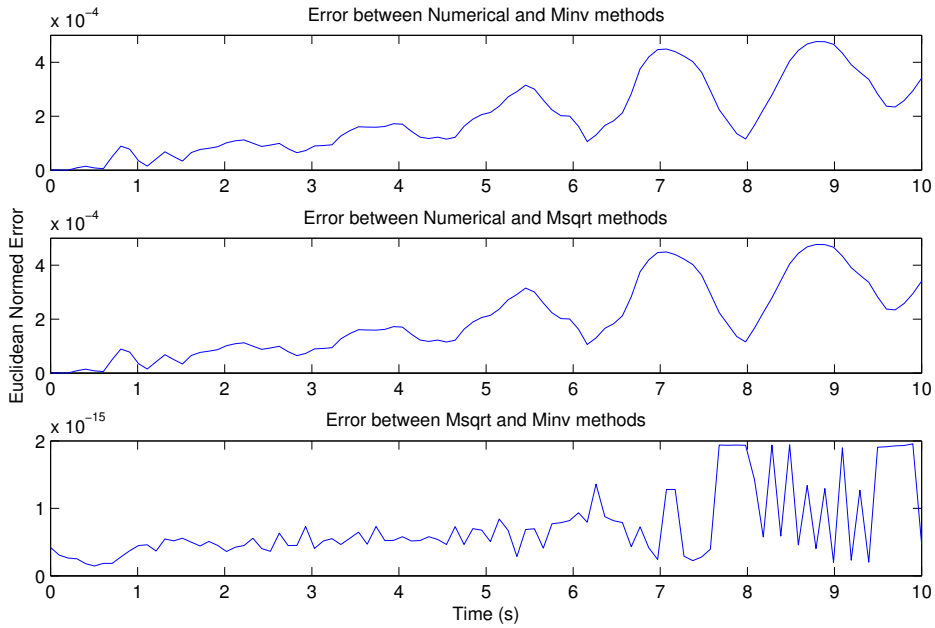
**Figure 13:** Solutions for a five mass system with a nonsingular  $K$  matrix using the methods described below that employ exponential functions to find the motion when  $K$  may be singular.



**Figure 14:** Associated error for the system in Figure 13



**Figure 15:** Solutions for a five mass system with a singular K matrix using the methods described below that employ exponential functions to find the motion when K may be singular.



**Figure 16:** Associated error for the system in Figure 15

Matlab code used to produce the above plots:

```
1 % Driver file
2
3 % n = 3;
4 % K = [2 -1 0; -1 2 -1; 0 -1 2]; % For K-nonsingular cases
5 % K = [1 -1 0; -1 2 -1; 0 -1 1]; % For K-singular cases
6
7 % Alternatives
8 n = 5;
9 % K = [3 -1 -1 0 0; -1 2 0 -1 0; -1 0 2 0 -1; 0 -1 0 2 -1; 0 0 -1 -1 3];
10 K = [2 -1 0 0 0; -1 2 -1 0 0; 0 -1 2 0 0; 0 0 0 1 -1; 0 0 0 -1 1];
11
12 M = eye(n);
13 x0 = rand(n,1)-.5; % Random initial conditions from -.5 to .5
14 v0 = rand(n,1)-.5;
15
16 tspan = linspace(0,10,1000);
17
18 % Get solutions
19 [~,xNum] = SpringmassNUM(tspan,x0,v0,K,M);
20
21 % K-Nonsingular methods
22 % [~,xMinv] = SpringmassMinv(tspan,x0,v0,K,M);
23 % [~,xMsqrt] = SpringmassSqrtM(tspan,x0,v0,K,M);
24
25 % K-Singular methods
26 % [~,xMinv] = SpringmassMinvKSingular(tspan,x0,v0,K,M);
27 % [~,xMsqrt] = SpringmassSqrtMKSingular(tspan,x0,v0,K,M);
28
29 % Exponential methods (handles K-singular)
30 [~,xMinv] = SpringmassMinvExponential(tspan,x0,v0,K,M);
31 [~,xMsqrt] = SpringmassSqrtMExponential(tspan,x0,v0,K,M);
32
33 % Error Analysis
34 errNumMinv = xNum-xMinv;
35 errNumMinv = sqrt(sum(errNumMinv.^2,2));
36
37 errNumMsqrt = xNum-xMsqrt;
38 errNumMsqrt = sqrt(sum(errNumMsqrt.^2,2));
39
40 errMsqrtMinv = xMsqrt-xMinv;
41 errMsqrtMinv = sqrt(sum(errMsqrtMinv.^2,2));
42
43 % Plot
44 figure(1)
45 clf
46 hNUM = plot(tspan',xNum);
47 hold on
48 hMinv = plot(tspan',xMinv,'x');
49 hMsqrt = plot(tspan',xMsqrt,'o');
50
51 xlabel('Time')
52 ylabel('Displacement from Equilibirum')
53
54 vecPrint = '';
55 Names = cell(1,n);
56 for i = 1:n
57     vecPrint = [vecPrint ' ', %3.2f']; %#ok<AGROW>
58     Names{i} = sprintf('Mass %d',i);
59 end
60 vecPrint = vecPrint(3:end);
61
```

```

62 title({sprintf('%d Mass System',n),...
63     sprintf(['x_0 = [' vecPrint ']' v_0 = [' vecPrint '']],x0,v0)})
64 legend([hNUM; hNUM(1); hMinv(2); hMsqrt(3)],Names{:},...
65     'Integrated Solution','Minv Solution','Msqrt Solution')
66
67 figure(2)
68 clf
69 subplot(3,1,1)
70 plot(tspan,errNumMinv)
71 title('Error between Numerical and Minv methods')
72 subplot(3,1,2)
73 plot(tspan,errNumMsqrt)
74 title('Error between Numerical and Msqrt methods')
75 ylabel('Euclidean Normed Error')
76 subplot(3,1,3)
77 plot(tspan,errMsqrtMinv)
78 title('Error between Msqrt and Minv methods')
79 xlabel('Time (s)')
80
81 % Animate
82 figure(3)
83 AnimateSolution(1:n,xNum,tspan)

```

**e Animate the solution (using moving dots, circles or squares, your choice).**

The following Matlab code will animate the solved spring mass system. It uses circles.

```

1 function AnimateSolution(x0,xarray,tspan)
2 % Animates an n-mass spring system's 1 dimensional motion in the current
3 % figure
4 %
5 % Inputs:
6 %   x0 - Array of equilibrium positions
7 %   xarray - Array of displacements for each mass in the system relative to
8 %           equilibrium. The i'th row corresponds to the positions at the
9 %           i'th time in tspan
10 %   tspan - array of times. tspan must include ALL time steps to be
11 %          plotted, not just the start and end times. The animation
12 %          assumes that all time steps in tspan are equal, and cannot
13 %          accurately animate a timestep shorter than .01s
14
15 nt = length(tspan);
16 n = size(xarray,2);
17
18 % Determine time step
19 dt = tspan(2)-tspan(1);
20
21 % Find absolute positions of the masses
22 xarray = xarray + repmat(x0(:)',nt,1);
23
24 xMax = max(max(xarray));
25 xMin = min(min(xarray));
26
27 % Set up plot
28 hArray = zeros(n,1);
29 hold on
30 for i = 1:n
31     hArray(i) = plot(xarray(1,i),0,'ko');

```

```

32 end
33 axis([xMin xMax -1 1]);
34
35 for i = 1:nt
36     for j = 1:n
37         set(hArray(j), 'XData', xarray(i, j));
38     end
39     pause(dt)
40 end

```

## 2 Extra things for 5730 students

a Make the functions above work even if  $K$  is singular (has some modes with zero frequency)

a.a `[tarray xarray] = SpringmassNUM(tspan, x0,v0,K,M)`

No changes are required.

a.b `[tarray xarray] = SpringmassMinv(tspan, x0,v0,K,M)`

If there exists some  $i$  for which  $\omega_i = 0$ , then Equation 8 is no longer valid. Instead, we have

$$\vec{x}(t) = \sum_{i \in \{i | \lambda_i \neq 0\}} \vec{v}_i (A_i \cos(\omega_i t) + B_i \sin(\omega_i t)) + \sum_{i \in \{i | \lambda_i = 0\}} \vec{v}_i (A_i + B_i t) \quad (21)$$

Equation 9 is still valid, but Equation 10 must be replaced by considering two cases. Since we see that, in either case,  $\vec{v}_0 \propto V\vec{B}$ , we will create an intermittent variable  $\vec{B}' = V^T \vec{v}_0$ .  $\vec{B}$  is related to  $\vec{B}'$  by

$$B_i = \begin{cases} \frac{B'_i}{\omega_i} & \lambda_i \neq 0 \\ B'_i & \lambda_i = 0 \end{cases} \quad (22)$$

Equations 9, 21, and 22 can be combined for the solution to Equation 1.

```

1 function [tarray xarray] = SpringmassMinvKSingular(tspan,x0,v0,K,M)
2 % Solves for the motion of the system defined by:
3 %     M(xddot) + K x = 0
4 % using eigenvectors of M^-1*K. Handles singular K matrices.
5 %
6 % Inputs:
7 %     M,K - Matrices as defined in the equation above
8 %     x0 - vector of initial positions
9 %     v0 - vector of initial velocities
10 %     tspan - times at which to output the state of the system. tspan must be
11 %         a vector of length >= 2. The simulation will begin at time in the
12 %         first element of tspan and end at the time in the last element.
13 % Outputs:
14 %     tarray - array of times corresponding to xarray
15 %     xarray - array of system states. The i'th row corresponds to the state
16 %         of the system at the i'th element in tspan

```



```

17
18 % Make IC vectors column
19 x0 = x0(:);
20 v0 = v0(:);
21
22 % Form timespan
23 if length(tspan) == 2
24     tarray = linspace(tspan(1),tspan(2));
25 else
26     tarray = tspan(:)';
27 end
28
29 [V,w2] = eig(M^-1*K);
30 w2 = diag(w2);
31 w2(abs(w2) < 1e-10) = 0;
32 w = sqrt(w2);
33
34 oM = w2~=0; % Oscillatory mode indices
35 rM = w2 == 0; % Rigid mode indices
36
37 % Solve for coefficients
38 A = V'*x0;
39 Bprime = V'*v0;
40 B = Bprime;
41 B(oM) = Bprime(oM)./w(oM); % Logical indexing, also used below
42
43 % Linear combination of the normal modes
44 % Because cos(0) = 1, we can use cospart even for the case of a rigid mode
45 cospart = repmat(A,1,length(tarray)).*cos(w*tarray);
46 % In order sin(0) = 0, but we need the rigid mode to have a t. We will have
47 % to break this out into two cases
48 sinpart(oM,:) = repmat(B(oM),1,length(tarray)).*sin(w(oM)*tarray);
49 sinpart(rM,:) = B(rM)*tarray;
50
51 x = V*(cospart + sinpart);
52 xarray = x';
53 end

```

**a.c** [tarray xarray] = SpringmassSqrtM(tspan, x0,v0,K,M)

The process of adjusting the modal solution for rigid modes is very similar to what we saw above. Equation 16 is no longer valid for all  $i$ . In particular, if we look at Equation 15 with  $\lambda_i = 0$ , we have  $\ddot{r}_i = 0$ , which implies a constant velocity solution. Our solution for the decoupled modes then becomes

$$r_i(t) = \begin{cases} C_i \cos(\sqrt{\lambda_i}t) + D_i \sin(\sqrt{\lambda_i}t) & \lambda_i \neq 0 \\ C_i + D_i t & \lambda_i = 0 \end{cases} \quad (23)$$

We now see that Equation 19 is still valid, while Equation 20 must be reformulated for two cases. Much like Equation 22, we have

$$D_i = \begin{cases} \frac{\dot{r}_{0,i}}{\sqrt{\lambda_i}} & \lambda_i \neq 0 \\ \dot{r}_{0,i} & \lambda_i = 0 \end{cases} \quad (24)$$

and we once again apply the transformation in Equation 18 to solve Equation 1.

```

1 function [tarray xarray] = SpringmassSqrtMKSingular(tspan,x0,v0,K,M)
2 % Solves for the motion of the system defined by:
3 %     M(xddot) + K x = 0
4 % using modal coordinates. Handles singular K matrices
5 %
6 % Inputs:
7 %     M,K – Matrices as defined in the equation above
8 %     x0 – vector of initial positions
9 %     v0 – vector of initial velocities
10 %     tspan – times at which to output the state of the system. tspan must be
11 %         a vector of length  $\geq 2$ . The simulation will begin at time in the
12 %         first element of tspan and end at the time in the last element.
13 % Outputs:
14 %     tarray – array of times corresponding to xarray
15 %     xarray – array of system states. The i'th row corresponds to the state
16 %         of the system at the i'th element in tspan
17
18 % Make IC vectors column
19 x0 = x0(:);
20 v0 = v0(:);
21
22 % For time span
23 if length(tspan) == 2
24     tarray = linspace(tspan(1),tspan(2));
25 else
26     tarray = tspan(:)';
27 end
28
29 Msqrt = M^(-1/2);
30 Ktwid = Msqrt*K*Msqrt;
31 [P,w2] = eig(Ktwid);
32 w2 = diag(w2);
33 w2(abs(w2) < 1e-10) = 0;
34 w = sqrt(w2);
35
36 oM = w2~=0; % Oscillitory mode indices
37 rM = w2 == 0; % Rigid mode indices
38
39 % Transform ICs
40 r0 = P'*Msqrt^-1*x0;
41 rd0 = P'*Msqrt^-1*v0;
42
43 % Solve for coefficients
44 C = r0;
45 D = rd0;
46 D(oM) = rd0(oM)./w(oM); % Logical indexing. Also used below.
47
48 % Find solution for each 1DOF oscillator
49 % Because cos(0) = 1, we can use cospart even for the case of a rigid mode
50 cospart = repmat(C,1,length(tarray)).*cos(w*tarray);
51 % In order sin(0) = 0, but we need the rigid mode to have a t. We will have
52 % to break this out into two cases
53 sinpart(oM,:) = repmat(D(oM),1,length(tarray)).*sin(w(oM)*tarray);
54 sinpart(rM,:) = D(rM)*tarray;
55
56 r = cospart + sinpart;
57
58 % Transform back to x-coordinates
59 x = M*P*r;
60 xarray = x';
61 end

```

**b** Instead of using cosine and sine for the normal modes, use exponentials and do complex math to solve for the initial conditions.

**b.a** [tarray xarray] = SpringmassNUM(tspan, x0,v0,K,M)

Not Applicable

**b.b** [tarray xarray] = SpringmassMinv(tspan, x0,v0,K,M)

We can begin from Equation 5, as we did for the solution using sines and cosines. This time, we assume a solution of the form

$$\vec{x}(t) = x(\omega t)\vec{v} = ae^{\omega t}\vec{v} \quad (25)$$

This results in the eigenvalue problem

$$(\omega^2 I + M^{-1}K)\vec{v} = 0 \quad (26)$$

which differs from what we had in Equation 7 by only a sign. As a result, we now have  $n$  eigenpairs  $(\lambda_i = \omega_i^2 < 0, \vec{v}_i)$ , which implies that the  $\omega_i$ 's are imaginary. Further, while we were previously able to take advantage of the odd/even properties of the sine and cosine functions to ignore the sign on  $\omega_i$ , we must now take into account both the positive and negative values. We now write our general solution:

$$\vec{x}(t) = \sum_{i=1}^n \vec{v}_i(a_i e^{\omega_i t} + b_i e^{-\omega_i t}) \quad (27)$$

If we wish to also factor in the case where  $K$  is singular, we note that  $\omega_i = -0 = +0$  behaves like a repeated root, and we find:

$$\vec{x}(t) = \sum_{i \in \{i|\lambda_i \neq 0\}} \vec{v}_i(a_i e^{\omega_i t} + b_i e^{-\omega_i t}) + \sum_{i \in \{i|\lambda_i = 0\}} \vec{v}_i(a_i + b_i t) \quad (28)$$

We note that the coefficients  $a_i$  and  $b_i$  are generally complex, while those having  $i \in \{i|\lambda_i = 0\}$  being purely real, since  $\vec{x}(t)$  is purely real. Applying our initial conditions, we have:

$$\vec{x}_0 = \sum_{i \in \{i|\lambda_i \neq 0\}} \vec{v}_i(a_i + b_i) + \sum_{i \in \{i|\lambda_i = 0\}} \vec{v}_i a_i \quad (29)$$

$$\vec{v}_0 = \sum_{i \in \{i|\lambda_i \neq 0\}} \vec{v}_i \omega_i (a_i - b_i) + \sum_{i \in \{i|\lambda_i = 0\}} \vec{v}_i b_i \quad (30)$$

Concerning only  $i \in \{i|\lambda_i \neq 0\}$ , we can see from Equation 29 that, since  $\vec{x}_0$  is real,  $a_i + b_i$  is real. Equivalently, we can say that the imaginary parts of  $a_i$  and  $b_i$  are opposite. Equation 30 similarly tells us that  $a_i - b_i$  is purely imaginary, since  $\omega_i$  is imaginary and  $\vec{v}_0$  real.

Equivalently, the real parts of  $a_i$  and  $b_i$  are equal. As such, we see that  $a_i$  and  $b_i$  are complex conjugates. The equations are now:

$$\vec{x}(t) = \sum_{i \in \{i|\lambda_i \neq 0\}} \vec{v}_i (a_i e^{\omega_i t} + a_i^* e^{-\omega_i t}) + \sum_{i \in \{i|\lambda_i = 0\}} \vec{v}_i (a_i + b_i t) \quad (31)$$

$$\vec{x}_0 = \sum_{i \in \{i|\lambda_i \neq 0\}} \vec{v}_i 2\text{Re}[a_i] + \sum_{i \in \{i|\lambda_i = 0\}} \vec{v}_i a_i = V^* \vec{a} \quad (32)$$

$$\vec{v}_0 = \sum_{i \in \{i|\lambda_i \neq 0\}} \vec{v}_i \omega_i 2\text{Im}[a_i] + \sum_{i \in \{i|\lambda_i = 0\}} \vec{v}_i b_i = V^{**} \vec{b} \quad (33)$$

The bookkeeping is somewhat tricky, but  $V^*$  and  $V^{**}$  both have columns that are multiples of linearly independent eigenvectors, and thus they are invertible. We can solve for  $\vec{a}$ , which contains the real parts of those  $a_i$  corresponding to oscillatory modes and the  $a_i$  for rigid modes, and  $\vec{b}$ , which contains the imaginary parts of those  $a_i$  corresponding to oscillatory modes and the  $b_i$  for rigid modes, by simple matrix operations. It is worth noting that a similar formulation would allow us to express Equation 22 as a matrix operation.

```

1 function [tarray xarray] = SpringmassMinvExponential (tspan,x0,v0,K,M)
2 % Solves for the motion of the system defined by:
3 %     M(xddot) + K x = 0
4 % using eigenvectors of M^-1*K. Handles singular K matrices. Uses
5 % exponential solutions.
6 %
7 % Inputs:
8 %   M,K - Matrices as defined in the equation above
9 %   x0 - vector of initial positions
10 %   v0 - vector of initial velocities
11 %   tspan - times at which to output the state of the system. tspan must be
12 %         a vector of length >= 2. The simulation will begin at time in the
13 %         first element of tspan and end at the time in the last element.
14 % Outputs:
15 %   tarray - array of times corresponding to xarray
16 %   xarray - array of system states. The i'th row corresponds to the state
17 %           of the system at the i'th element in tspan
18
19 % Make IC vectors column
20 x0 = x0(:);
21 v0 = v0(:);
22
23 % Form timespan
24 if length(tspan) == 2
25     tarray = linspace(tspan(1),tspan(2));
26 else
27     tarray = tspan(:)';
28 end
29
30 [V,w2] = eig(M^-1*K);
31 w2 = diag(w2);
32 w2(abs(w2) < 1e-10) = 0;
33 w = sqrt(-w2);
34
35 oM = w2~=0; % Oscillatory mode indices
36 rM = w2 == 0; % Rigid mode indices
37

```

```

38 % Solve for coefficients
39 Vstar(:,oM) = 2*V(:,oM); % Logical indexing. Used throughout.
40 Vstar(:,rM) = V(:,rM);
41 a = Vstar^-1*x0;
42
43 Vsstar(:,oM) = 2*V(:,oM).*repmat(w(oM)'/1j,length(w),1);
44 Vsstar(:,rM) = V(:,rM);
45 b = Vsstar^-1*v0;
46
47 % Linear combination of the normal modes
48 pospart = zeros(length(w),length(tarray));
49 pospart(oM,:) = repmat(a(oM) + b(oM)*1j,1,length(tarray)).*exp(w(oM)*tarray);
50
51 negpart = zeros(length(w),length(tarray));
52 negpart(oM,:) = repmat(a(oM) - b(oM)*1j,1,length(tarray)).*exp(-w(oM)*tarray);
53
54 constpart = zeros(length(w),length(tarray));
55 constpart(rM,:) = repmat(a(rM),1,length(tarray));
56
57 linpart = zeros(length(w),length(tarray));
58 linpart(rM,:) = b(rM)*tarray;
59
60 x = V*(pospart + negpart + constpart + linpart);
61 xarray = x';
62 end

```

### b.c [tarray xarray] = SpringmassSqrtM(tspan, x0,v0,K,M)

We now start with Equation 15, and now assume solutions

$$r_i(t) = c_i e^{\omega_i t} \quad (34)$$

and find that  $\omega_i = \pm\sqrt{-\lambda_i}$ . If we apply the above process used for the MDOF system to each of our decoupled SDOF modes, we will find the solutions:

$$r_i(t) = \begin{cases} c_i e^{\omega_i t} + c_i^* e^{-\omega_i t} & \lambda_i \neq 0 \\ c_i + d_i t & \lambda_i = 0 \end{cases} \quad (35)$$

and by applying the initial conditions we get:

$$r_{0,i} = \begin{cases} 2\text{Re}[c_i] & \lambda_i \neq 0 \\ c_i & \lambda_i = 0 \end{cases} \quad (36)$$

$$\dot{r}_{0,i} = \begin{cases} 2\omega_i \text{Im}[c_i] & \lambda_i \neq 0 \\ d_i & \lambda_i = 0 \end{cases} \quad (37)$$

which can be solved in each individual case by simple rearrangement. Once again, we apply the transformation in Equation 18.

```

1 function [tarray xarray] = SpringmassSqrtMExponential(tspan,x0,v0,K,M)
2 % Solves for the motion of the system defined by:
3 % M(xddot) + K x = 0
4 % using modal coordinates. Handles singular K matrices. Uses
5 % exponential solutions.

```

```

6 %
7 % Inputs:
8 %   M,K – Matrices as defined in the equation above
9 %   x0 – vector of initial positions
10 %   v0 – vector of initial velocities
11 %   tspan – times at which to output the state of the system. tspan must be
12 %           a vector of length  $\geq 2$ . The simulation will begin at time in the
13 %           first element of tspan and end at the time in the last element.
14 % Outputs:
15 %   tarray – array of times corresponding to xarray
16 %   xarray – array of system states. The i'th row corresponds to the state
17 %           of the system at the i'th element in tspan
18
19 % Make IC vectors column
20 x0 = x0(:);
21 v0 = v0(:);
22
23 % For time span
24 if length(tspan) == 2
25     tarray = linspace(tspan(1),tspan(2));
26 else
27     tarray = tspan(:)';
28 end
29
30 Msqrt = M^(-1/2);
31 Ktwid = Msqrt*K*Msqrt;
32 [P,w2] = eig(Ktwid);
33 w2 = diag(w2);
34 w2(abs(w2) < 1e-10) = 0;
35 w = sqrt(-w2);
36
37 oM = w2~=0; % Oscillatory mode indices
38 rM = w2 == 0; % Rigid mode indices
39
40 % Transform ICs
41 r0 = P'*Msqrt^-1*x0;
42 rd0 = P'*Msqrt^-1*v0;
43
44 % Solve for coefficients
45 c(oM) = r0(oM)/2; % Logical indexing, used throughout
46 c(rM) = r0(rM);
47 c = c(:); % logical indexing creates a row vector, make it a column
48 d(oM) = rd0(oM)./(2*w(oM)*1j);
49 d(rM) = rd0(rM);
50 d = d(:); % logical indexing creates a row vector, make it a column
51
52 % Solution for each oscillator
53 pospart = zeros(length(w),length(tarray));
54 pospart(oM,:) = repmat(c(oM) + d(oM)*1j, 1,length(tarray)).*exp(w(oM)*tarray);
55
56 negpart = zeros(length(w),length(tarray));
57 negpart(oM,:) = repmat(c(oM) - d(oM)*1j, 1,length(tarray)).*exp(-w(oM)*tarray);
58
59 constpart = zeros(length(w),length(tarray));
60 constpart(rM,:) = repmat(c(rM),1,length(tarray));
61
62 linpart = zeros(length(w),length(tarray));
63 linpart(rM,:) = d(rM)*tarray;
64
65 r = pospart + negpart + constpart + linpart;
66
67 % Transform back to x-coordinates
68 x = M*P*r;
69 xarray = x';
70 end

```

---